



NC020

FILTER & CAPACITOR BANK PROTECTION RELAY
THE LOW COST SOLUTION
FOR HARMONIC FILTERS AND CAPACITOR BANK

— Application

In recent years the harmonic producing part of total load has increased continuously because of the massive usage of power electronic in all the voltage levels. Thyristor convertors, frequency convertors, thyristor switches and static var compensator, such as thyristor controlled reactors (TCR) and thyristor switched capacitors (TSC), are commonly adopted in industrial applications and power utilities.

Filter capacitor banks consist of capacitor bank and series connected air core. Their task is to absorb the harmonic currents generated by loads and all above mentioned power electronic devices.

The aim of NC020 is to provide a reliable and cost effective solution for such an application granting capacitor bank safe operations.

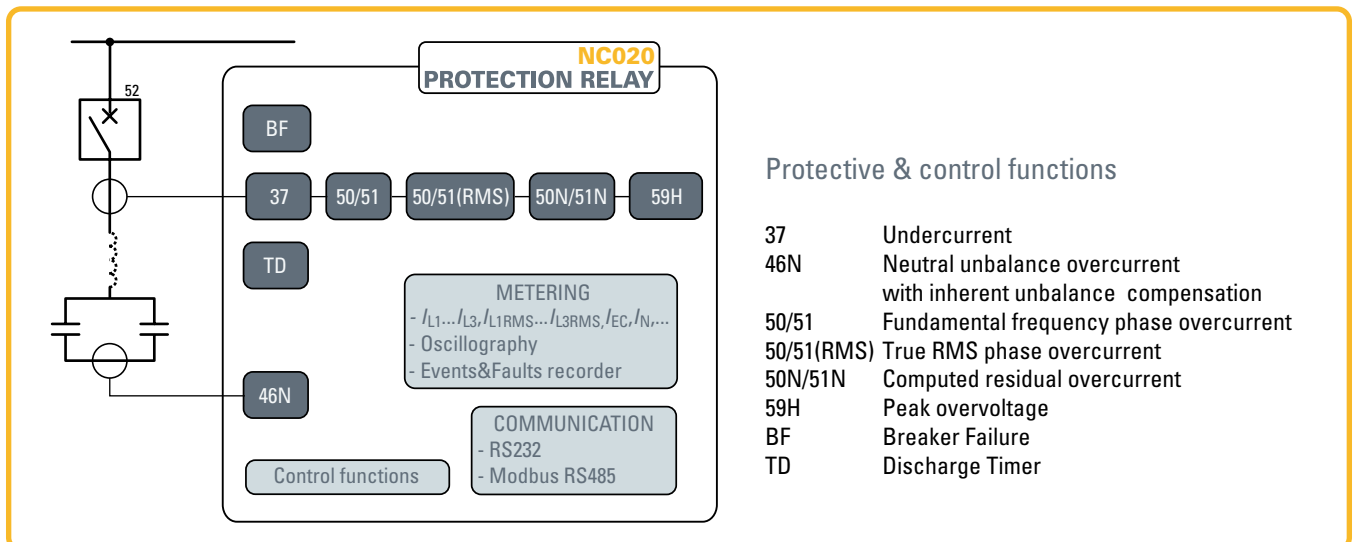
The capacitor banks may have the following configurations:

- Single Wye grounded.
- Single Wye ungrounded (with a resistor on the output of the neutral unbalance voltage transformer in order to develop the appropriate input current for the unbalance protection).
- Double Wye ungrounded.

A suitable compensation method is provided to compensate the inherent unbalance neutral current.

Protection 50/51 RMS is based on true RMS value measurement of the three phase currents (fundamental and harmonics up to the 23th).

The peak capacitor voltage is achieved for any phase by means of the sum of the fundamental frequency voltage and its harmonics (up to twenty-third order), calculated from the phase currents. Hence it is an innovative key against the dangerous pick voltages for those applications without VTs for the direct measurement of the capacitor voltages.



SPECIFICATIONS

GENERAL

— Mechanical data	
Mounting:	flush, rack
Mass (flush mounting case)	1.2 kg
— Insulation tests	
Reference standards	EN 60255-5
High voltage test 50Hz	2 kV 60 s
Impulse voltage withstand (1.2/50 μ s)	5 kV
Insulation resistance	>100 M Ω
— Voltage dip and interruption	
Reference standards	EN 61000-4-29
— EMC tests for interference immunity	
1 MHz damped oscillatory wave	EN 60255-22-1 1 kV-2.5 kV
Electrostatic discharge	EN 60255-22-2 8 kV
Fast transient burst (5/50 ns)	EN 60255-22-4 4 kV
Conducted radio-frequency fields	EN 60255-22-6 10 V
Radiated radio-frequency fields	EN 60255-4-3 10 V/m
High energy pulse	EN 61000-4-5 2 kV
Magnetic field 50 Hz	EN 61000-4-8 1 kA/m
Damped oscillatory wave	EN 61000-4-12 2.5 kV
Ring wave	EN 61000-4-12 2 kV
Conducted common mode (0...150 kHz)	EN 61000-4-16 10 V
— Emission	
Reference standards	EN 61000-6-4 (ex EN 50081-2)
Conducted emission 0.15...30 MHz	Class A
Radiated emission 30...1000 MHz	Class A
— Climatic tests	
Reference standards	IEC 60068-x, ENEL R CLI 01, CEI 50
— Mechanical tests	
Reference standards	EN 60255-21-1, 21-2, 21-3
— Safety requirements	
Reference standards	EN 61010-1
Pollution degree	3
Reference voltage	250 V
Overvoltage	III
Pulse voltage	5 kV
Reference standards	EN 60529
Protection degree:	
• Front side	IP52
• Rear side, connection terminals	IP20
— Environmental conditions	
Ambient temperature	-25...+70 °C
Storage temperature	-40...+85 °C
Relative humidity	10...95 %
Atmospheric pressure	70...110 kPa
— Certifications	
Product standard for measuring relays	EN 50263
CE conformity	
• EMC Directive	2004/108/EC
• Low Voltage Directive	2006/95/EC
Type tests	IEC 60255-6

COMMUNICATION INTERFACES

Local PC RS232	19200 bps
RS485 port	1200...57600 bps
Protocol	ModBus® RTU

INPUT CIRCUITS

— Rated frequency	
Rated value ⁽¹⁾	50 or 60 Hz
<i>Note 1 - Must be selected at time of order</i>	
— Auxiliary power supply Uaux	
Nominal value (range)	24...230 Vac/dc
Operative range	19...265 Vac / 19...300 Vdc
Power consumption (max)	6 W (9 VA)
— Phase current inputs	
Nominal current I_n	1 A or 5 A selectable by DIP Switches
Permanent overload	25 A
Thermal overload (1 s)	500 A
Rated consumption (for any phase)	≤ 0.002 VA ($I_n = 1$ A) ≤ 0.04 VA ($I_n = 5$ A)
Connections	4 mm ring lugs suitable for M4 screws
— Unbalanced neutral current input	
Nominal current I_{Nn}	1 A or 5 A selectable by DIP Switch
Permanent overload	25 A
Thermal overload (1 s)	500 A
Rated consumption	≤ 0.006 VA ($I_{Nn} = 1$ A) ≤ 0.012 VA ($I_{Nn} = 5$ A)
Connections	4 mm ring lugs suitable for M4 screws
— Binary inputs	
Quantity	3
• IN1	52b
• IN2	52a
• IN3	Remote Reset
Type	dry inputs
Max permissible voltage	19...265 Vac/19...300 Vdc
Max consumption, energized	3 mA

OUTPUT CIRCUITS

— Output relays K1...K4	
Quantity	4
Command relays K1, K2, K4	
Type of contacts	changeover (SPDT, type C)
Nominal current	8 A
Nominal voltage/max switching voltage	250 Vac/400 Vac
Breaking capacity:	
• Direct current (L/R = 40 ms)	50 W
• Alternating current ($\lambda = 0,4$)	1250 VA
Make	1000 W/VA
Short duration current (0,5 s)	30 A
Signalling relays K3	
Type of contacts	changeover (SPDT, type C)
Nominal current	8 A
Nominal voltage/max switching voltage	250 Vac/400 Vac
— LEDs	
Quantity	8
• ON/fail (green)	1
• Start (yellow)	1
• Trip (red)	1
• Trip I>, I>>, I>>> RMS or DFT (red)	1
• Trip 46N, 50N (red)	1
• Trip 59H (red)	1
• CB position (red)	1
• TD state (red)	1

GENERAL SETTINGS

— Rated values	
Phase CT nominal primary current (I_{np})	1 A...5000 A
Neutral CT nominal primary current (I_{Nnp})	1 A...5000 A
Reading	Direct / Relative
— Relay output timers	
Minimum pulse width (t_{TR})	0.01...0.50 s

PROTECTIVE FUNCTIONS

— Discharge time (TD)

TD discharge time (t_D) 6...6000 s

Note - When enabled it is started by the internal threshold of the undercurrent protection (37). The discharge time counter may be manually cleared by MMI command and by ThyVisor

— Compensation - 46N

Compensation current ($I_{NC\ MOD\ calib}$) - I_{Nn}
 Compensation angle ($I_{NC\ PHI\ calib}$) °

Note - The compensation parameters are determined by the device as a result of the command "INC Comp exe" that must be activated in the Commands\Compensation\Set compensation menu

— Undercurrent - 37

I< Element

Definite time

- First threshold definite time ($I_{<def}$) 0.1 I_n
- $I_{<def}$ Operating time ($t_{<def}$) 0.100 s

I<< Element

Definite time

- second threshold definite time ($I_{<<def}$) 0.05...1.00 I_n
- $I_{<<def}$ Operating time ($t_{<<def}$) 0.03...600 s

Note - The 37 element is based on RMS measurement of three phase currents (the computed RMS value takes into account the contribution of fundamental and harmonics). It is an internal element servicing the Timer Discharge (TD) function.

— Neutral unbalance overcurrent - 46N

I>AL Element

- $I_{NCLP>AL}$ CLP activation time 0.00...100.0 s

Definite time

- 46N Alarm threshold definite time ($I_{N>ALdef}$) 0.01...2.00 I_{Nn}
- $I_{N>ALdef}$ within CLP ($I_{NCLP>ALdef}$) 0.01...2.00 I_{Nn}
- $I_{N>ALdef}$ Operating time ($t_{N>ALdef}$) 0.03...600 s

I> Element

- $I_{N>}$ CLP activation time ($t_{NCLP>}$) 0.00...100.0 s

Definite time

- 46N First threshold definite time ($I_{N>def}$) 0.01...2.00 I_{Nn}
- $I_{N>def}$ within CLP ($I_{NCLP>def}$) 0.01...2.00 I_{Nn}
- $I_{N>def}$ Operating time ($t_{N>def}$) 0.03...600 s

I>> Element

- $I_{N>>}$ CLP activation time ($t_{NCLP>>}$) 0.00...100.0 s

Definite time

- 46N Second threshold definite time ($I_{N>>def}$) 0.01...2.00 I_{Nn}
- $I_{N>>def}$ within CLP ($I_{NCLP>>def}$) 0.01...2.00 I_{Nn}
- $I_{N>>def}$ Operating time ($t_{N>>def}$) 0.03...60.0 s

— Phase overcurrent - 50/51 RMS ^[1]

I> Element

- *I*> Curve type (*I*>Curve) DEFINITE
IEC/BS A, B, C, ANSI/IEEE MI, VI, EI, CAPACITOR ^[2]

- *I*> CLP activation time ($t_{CLP>}$) 0.00...100.0 s
- *I*> Reset time delay ($t_{>RES}$) 0.00...100.0 s

Definite time

- 50/51 RMS First threshold definite time ($I_{>def}$) 0.100...20.0 I_n
- $I_{>def}$ within CLP ($I_{CLP>def}$) 0.100...20.0 I_n
- $I_{>def}$ Operating time ($t_{>def}$) 0.03...600 s

Inverse time

- 50/51 First threshold inverse time ($I_{>inv}$) 0.100...2.50 I_n
- $I_{>inv}$ within CLP ($I_{CLP>inv}$) 0.100...10.00 I_n
- $I_{>inv}$ Operating time ($t_{>inv}$) 0.02...60.0 s

Note [1] - The 50/51 RMS protection is based on RMS value measurement of three phase currents (the computed RMS value takes into account the contribution of fundamental and harmonic up to twenty-third order)

Note [2] - The mathematical formula for CAPACITOR curves is:

$$t = \frac{t_{>inv} \cdot 50000}{[1.1 \cdot (I_{RMS}/I_{>inv})^{17}-1]} + 0.1$$

where:

t = trip time (in seconds)

$t_{>inv}$ = operating time setting (in seconds)

I_{RMS} = input current

$I_{>inv}$ = threshold setting

— Phase overcurrent - 50/51 Fundamental

I>> Element

- *I*>> Curve type (*I*>>Curve) DEFINITE
IEC/BS A, B, C, ANSI/IEEE MI, VI, EI, CAPACITOR

- *I*>> CLP activation time ($t_{CLP>>}$) 0.00...100.0 s
- *I*>> Reset time delay ($t_{>>RES}$) 0.00...100.0 s

Definite time

- 50/51 Second threshold definite time ($I_{>>def}$) 0.100...20.0 I_n
- $I_{>>def}$ within CLP ($I_{CLP>>def}$) 0.100...20.0 I_n
- $I_{>>def}$ Operating time ($t_{>>def}$) 0.03...600 s

Inverse time

- 50/51 Second threshold inverse time ($I_{>>inv}$) 0.100...2.50 I_n
- $I_{>>inv}$ within CLP ($I_{CLP>>inv}$) 0.100...10.00 I_n
- $I_{>>inv}$ Operating time ($t_{>>inv}$) 0.02...60.0 s

I>>> Element

- $I_{CLP>>>}$ CLP activation time ($t_{CLP>>>}$) 0.00...100.0 s
- *I*>>> Reset time delay ($t_{>>>RES}$) 0.00...100.0 s

Definite time

- 50/51 Third threshold definite time ($I_{>>>def}$) 0.100...20.0 I_n
- $I_{>>>def}$ within CLP ($I_{CLP>>>def}$) 0.100...20.0 I_n
- $I_{>>>def}$ Operating time ($t_{>>>def}$) 0.03...60.0 s

— Residual overcurrent - 50N/51N

*I*E> Element

- $I_E>$ CLP activation time ($t_{IECLP>}$) 0.00...100.0 s
- $I_E>$ Reset time delay ($t_{E>RES}$) 0.00...100.0 s

Definite time

- 50N/51N First threshold definite time ($I_{E>def}$) 0.100...10.00 I_n
- $I_{E>def}$ within CLP ($I_{ECLP>def}$) 0.100...10.00 I_n
- $I_{E>def}$ Operating time ($t_{E>def}$) 0.03...200 s

*I*E>> Element

- $I_E>>$ CLP activation time ($t_{IECLP>>}$) 0.00...100.0 s
- $I_E>$ Reset time delay ($t_{E>>RES}$) 0.00...100.0 s

Definite time

- 50N/51N Second threshold definite time ($I_{E>>def}$) 0.100...10.00 I_n
- $I_{E>>def}$ within CLP ($I_{ECLP>>def}$) 0.100...10.00 I_n
- $I_{E>>def}$ Operating time ($t_{E>>def}$) 0.03...60.0 s

Note: The computed residual current I_{EC} (vectorial sum of the phase currents) is employed

— Peak overvoltage - 59H

U> Element

- *U*> CLP activation time ($t_{UCLP>}$) 0.00...100.0 s
- *U*> Reset time delay ($t_{U>RES}$) 0...600 s

Definite time

- 59 First threshold definite time ($U_{>def}$) 0.20...10.00 U_n
- $U_{>def}$ within CLP ($U_{CLP>def}$) 0.20...10.00 U_n
- $U_{>def}$ Operating time ($t_{U>def}$) 0.03...600 s

U>> Element

- $U_{>>}$ CLP activation time ($t_{UCLP>>}$) 0.00...100.0 s
- $U_{>>}$ Reset time delay ($t_{U>>RES}$) 0...600 s

Definite time

- 59 Second threshold definite time ($U_{>>def}$) 0.20...10.00 U_n
- $U_{>>def}$ within CLP ($U_{CLP>>def}$) 0.20...10.00 U_n
- $U_{>>def}$ Operating time ($t_{U>>def}$) 0.03...200 s

U>>> Element

- $U_{>>>}$ CLP activation time ($t_{UCLP>>>}$) 0.00...100.0 s
- $U_{>>>}$ Reset time delay ($t_{U>>>RES}$) 0...600 s

Definite time

- 59 Third threshold definite time ($U_{>>>def}$) 0.20...10.00 U_n
- $U_{>>>def}$ within CLP ($U_{CLP>>>def}$) 0.20...10.00 U_n
- $U_{>>>def}$ Operating time ($t_{U>>>def}$) 0.03...60.0 s

Note - The 59H element is based on calculation of peak voltages (the computed value is obtained from currents taking into account the contribution of fundamental and harmonic up to twenty-third order)

— Circuit Breaker supervision

CB check 52a, 52b, 52a/52b

— Breaker failure - BF

BF Enable Trip *I*>, *I*>>, *I*>>>, *I*E>, *I*E>>, *I*N>AL, *I*N>, *I*N>>, *U*>...
 Time delay (t_{BF}) 0.10...10.00 s

METERING & RECORDING

— Measures

• Fundamental RMS phase currents	I_{L1}, I_{L2}, I_{L3}
• RMS phase currents	$I_{L1 \text{ RMS}}, I_{L2 \text{ RMS}}, I_{L3 \text{ RMS}}$
• Fundamental RMS calculated residual current	I_{EC}
• Fundamental RMS of neutral current	I_N
• Displacement angle of neutral current	$I_N \text{ PHI}$
• Fundamental RMS of compensated neutral current	I_{NC}
• Displacement angle of calibrated neutral current	$I_{N \text{ PHI calib}}$
• Fundamental RMS of calibrated neutral current	$I_{NC \text{ MOD calib}}$
• Capacitor calculated peak voltages (p.u.)	V_1, V_2, V_3
• Discharge timer	T_D

— Circuit Breaker

• Position	Open - Close - Unknown
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— Digital inputs

• IN1 - 52b state	On/Off
• IN2 - 52a state	On/Off
• IN3 - Remote Reset	On/Off

— Counters

• Start I> element	On/Off
• Start I>> element	On/Off
• Start I>>> element	On/Off
• Start IE> element	On/Off
• Start IE>> element	On/Off
• Start IN>AL element	On/Off
• Start IN> element	On/Off
• Start IN>> element	On/Off
• Start U> element	On/Off
• Start U>> element	On/Off
• Start U>>> element	On/Off
• Start I<< element	On/Off
• Trip > element	On/Off
• Trip I>> element	On/Off
• Trip I>>> element	On/Off
• Trip IE> element	On/Off
• Trip IE>> element	On/Off
• Trip IN>AL element	On/Off
• Trip IN> element	On/Off
• Trip IN>> element	On/Off
• Trip U> element	On/Off
• Trip U>> element	On/Off
• Trip U>>> element	On/Off
• Trip I<< element	On/Off

— Event recorder

Number of events	50
Recording mode	circular

Trigger:

• Output relays switching	K1...K4
• Binary inputs switching	IN1, IN2, IN3

Data recorded:

• Event counter (resettable by ThyVisor)	0...10 ⁹
• Event cause	binary input/output relay/setting changes
• Time stamp	Date and time

— Fault recorder

Number of events	20
Recording mode	circular

Trigger:

• Output relays activation (OFF-ON transition)	K1...K4
• External trigger (binary inputs)	IN1, IN2, IN3
• Element pickup (OFF-ON transition)	Start/Trip

Data recorded:

• Event counter (resettable by ThyVisor)	0...10 ⁹
• Fundamental RMS phase currents	I_{L1}, I_{L2}, I_{L3}
• RMS phase currents	$I_{L1 \text{ RMS}}, I_{L2 \text{ RMS}}, I_{L3 \text{ RMS}}$
• Fundamental RMS calculated residual current	I_{EC}
• Fundamental RMS of compensated current	I_{NC}
• Capacitor peak voltages	V_1, V_2, V_3
• Fault cause	start, trip
• Fault cause info (operating phase)	L1, L2, L3
• Time stamp	Date and time

— Digital Fault Recorder (Oscillography)^[1]

File format	COMTRADE
Records	2 ^[2]
Recording mode	circular
Sampling rate	24 per power frequency cycle

Trigger setup

• Pre-trigger time	0...63 T ^[3]
• Trigger from inputs	IN1, IN2, IN3
• Trigger from outputs	K1...K4
• General trigger from start / trip	Start, Trip
• Manual trigger	ThyVisor
• Trigger from start / trip	Start I>, I>>, ... Trip I>...
• Manual trigger	

• Data recorded on analog channels (Analog 1...4)

• Instantaneous currents	$i_{L1}, i_{L2}, i_{L3}, i_N$
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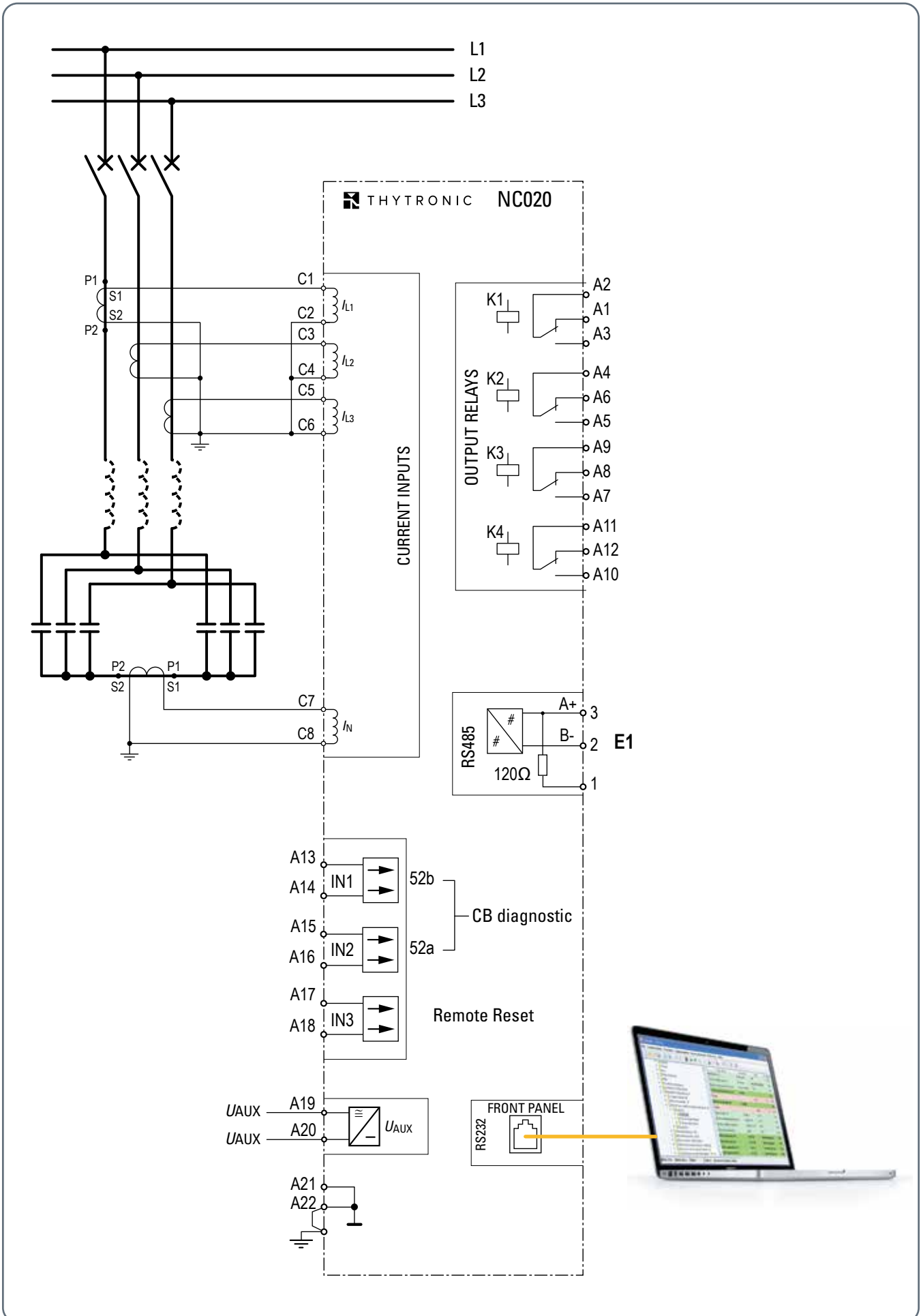
Data recorded on digital channels (Digital 1...4)

• Binary inputs state	IN1, IN2, IN3
• Output relays state	K1...K4
• General trigger from start / trip	Start, Trip

Note 1 - The oscillographic records are stored in non-volatile memory

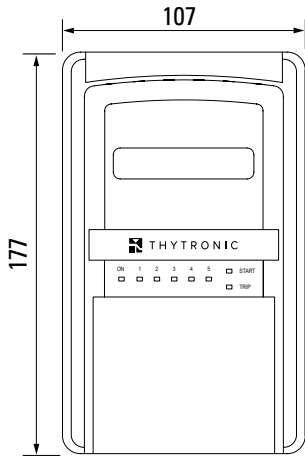
Note 2 - the time duration of the two records is dependent of settings

— Example of connection diagram

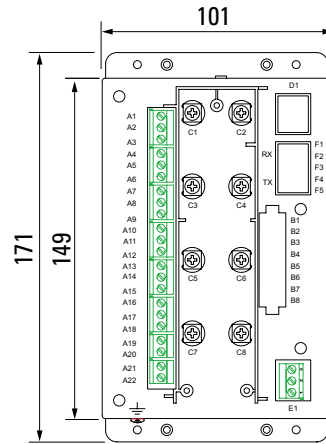


DIMENSIONS

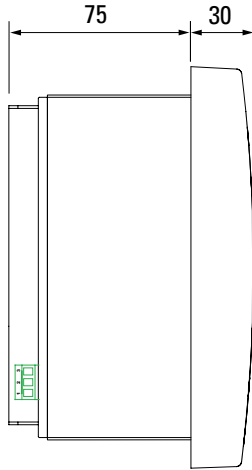
FRONT VIEW



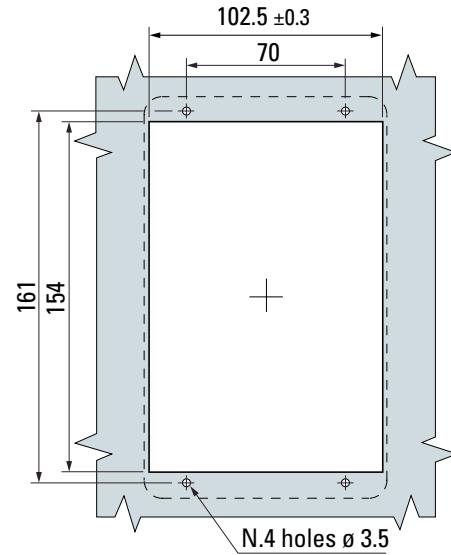
REAR VIEW



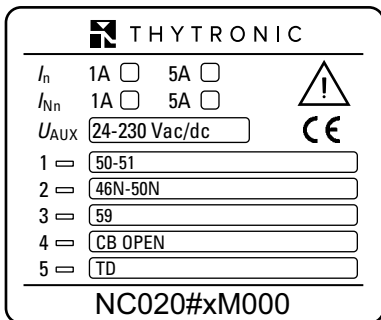
SIDE VIEW



FLUSH MOUNTING CUTOUT



IDENTIFICATION LABEL



LEDs



- ON: powered device and diagnostics OK
- START: start of any element
- TRIP: trip of any element
- LED 1: Trip of the I>, I>>, I>>> elements (RMS or DFT)
- LED 2: Trip of the 50N, 46N elements
- LED 3: Trip of the 59H element
- LED 4: CB Open (CB position)
- LED 5: TD state



THYTRONIC
ENERGY FOR A SAFER FUTURE

A PERSONALISED SERVICE OF THE PRODUCTION, A RAPID DELIVERY, A COMPETITIVE PRICE AND AN ATTENTIVE EVALUATION OF OUR CUSTOMERS NEEDS, HAVE ALL CONTRIBUTED IN MAKING US ONE OF THE BEST AND MOST RELIABLE PRODUCERS OF PROTECTIVE RELAYS. FORTY YEARS OF EXPERIENCE HAS MADE STANDARD THESE ADVANTAGES THAT ARE GREATLY APPRECIATED BY LARGE COMPANIES THAT DEAL ON THE INTERNATIONAL MARKET. A HIGHLY QUALIFIED AND MOTIVATED STAFF PERMITS US TO OFFER AN AVANT-GARDE PRODUCT AND SERVICE WHICH MEET ALL SAFETY AND CONTINUITY DEMANDS, VITAL IN THE GENERATION OF ELECTRIC POWER. OUR COMPANY PHILOSOPHY HAS HAD A POSITIVE REACTION FROM THE MARKET BY BACKING OUR COMMITMENT AND HENCE STIMULATING OUR GROWTH.

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